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(54) **Surface-treated wire for use in composite elements of elastomeric material and manufacturing process therefore**

Oberflächlich behandelter Draht zur Verwendung in Verbundteilen aus elastomerem Werkstoff und Herstellungsverfahren dafür

Fil traité en surface utilisé pour pièces composites en matière élastomère et procédé pour sa fabrication

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Description

The present invention relates to a wire, generally a steel wire, provided with a surface coating of a metal alloy. The invention also relates to a process put into practice for carrying out surface-treating of the wire in question and a composite element obtained by incorporating wires made in accordance with the present invention into an elastomeric matrix.

It is known that in the manufacture of rubber articles, such as tyres for motor-vehicles and the like, composite structural elements are widely used, that is elements made up of a matrix of an elastomeric material into which a plurality of wires or metallic cords each consisting of a plurality of said wires are incorporated, the function of which is to give the structural element the necessary features in terms of structural strength and geometrical stability.

The wires used for this purpose, generally steel wires, are obtained as a result of a drawing operation carried out at several different times as far as the desired size is reached, and usually have a coating of a metal alloy on their surface, the essential functions of said coating consisting in promoting the drawing capability of the wire and the adhesion of the elastomeric matrix to the wire itself.

To this end, different modalities for making the wire coating have been proposed.

For example, the European Patent EP 296,036 deals with a wire coating made of copper, brass, tin, zinc or alloys thereof also containing nickel or cobalt for the purpose of improving adhesion of the elastomeric material to the wire.

In the European Patent EP 283,738, filed in the name of the same Applicant, a wire coating is disclosed which consists of two superposed layers made of a nickel/zinc alloy wherein, in the inner layer, the zinc content is included between 60% and 90% and in the outer layer the nickel content is in the range of 60% to 80%. In the same patent the possibility of replacing nickel with cobalt in the nickel/zinc alloy is suggested.

In French patents FR 2,413,228 and FR 2,426,562 a wire coated with a ternary alloy consisting of brass and cobalt is described, in which the cobalt content is included between 0.5% and 30%.

In US Patent 2,296,838 the wire coating consists of an inner layer and an outer layer, made of zinc and cobalt respectively.

US Patent 4,218,517 illustrates the application to a wire of a coating made of a copper/cobalt alloy in which the copper content is in the range of 10% to 70%.

Finally, US Patent 4,872,932 pertains to a method of making composite elements of an elastomeric material essentially consisting of a support and a matrix of an elastomeric material fastened thereto. In this manufacturing method a film of a thickness included between 10 Å and 100 µm, made of a zinc/cobalt alloy with a cobalt content higher than 80% is provided to be deposited on said support.

In accordance with the present invention, it has been found that if the coating is carried out by electrodeposition of a zinc/cobalt alloy having a cobalt content not higher than 1%, optimal features in terms of drawing capability and corrosion strength of the wire can be simultaneously achieved, as well as an excellent adhesion of the matrix of elastomeric material to the wires, the attachment values being high even after aging of the composite element.

In particular, the invention relates to a surface treated wire, adapted to make composite elements of elastomeric material, characterized in that said surface coating consists of a zinc/cobalt alloy having a cobalt content lower than 1%.

Preferably said coating is obtained by electrodeposition of the coating layer on the wire surface, and the cobalt content in the coating layer is lower than 0.5%.

In the coating layer of the drawn wire which has a thickness included between 0.1 µm and 0.6 µm two different concentration levels of the cobalt material can be distinguished and more particularly a level included between 2% and 3% at the radially inner area, that is that directly in contact with the bare wire and a level lower than 0.5% in the radially outer area.

Advantageously, said steel wire has a carbon content included between 0.6% and 0.9% and a diameter after drawing in the range of 0.10 mm to 0.50 mm.

It is also an object of the present invention to provide a process for making a surface treated wire, especially adapted for use with composite elements of elastomeric material, characterized in that it comprises an immersion step of the wire into an electrolytic bath containing cobalt sulfate and zinc sulfate, in order to carry out the deposition of a zinc/cobalt alloy on the wire itself, said alloy exhibiting a cobalt content lower than 1%.

Preferably, the electrolytic bath is made up of an aqueous solution containing zinc sulfate heptahydrate in an amount included between 600 and 630 g/l, cobalt sulfate heptahydrate in an amount included between 100 and 110 g/l, as well as sodium sulfate in an amount included between 70 and 80 g/l.

In a preferential solution the electrolytic bath, maintained to a temperature in the range of 25° to 35°C, is passed through by the wire being worked at a rate of 15 to 25 meters/minute and the residence time of the wire in the electrolytic bath has a duration of 5 to 15 seconds.

In an alternative embodiment the electrolytic bath, maintained to a temperature in the range of 50° to 60°C is passed through by the wire being worked at a rate of 40 to 60 meters/minute and the residence time of the wire in the electrolytic bath has a duration of 2 to 6 seconds.

The electrolytic bath preferably has a pH included between 1.5 and 2.5, at 55°C, the value of said pH being adjusted by addition of sulphuric acid.

Referring to a preferential solution, a cathodic current of a density included between 30 and 40 ampere per square decimetre (A/dm²) is applied to the wire being worked, whereas in the cited alternative embodiment a cathodic current of a density included between 65 and 85 A/dm² is applied to said wire.

The process further comprises at least one drawing step carried out on the wire provided with the coating layer made up of a zinc/cobalt metal alloy, the wire diameter being of a value included between 1.2 mm and 1.6 mm before drawing and of a value included between 0.10 mm and 0.50 mm after drawing.

After drawing the thickness of the coating layer is in the range of 0.1 µm to 0.6 µm.

It is a further object of the present invention to provide a composite element comprising a matrix of an elastomeric material and reinforcing steel wires or cords provided with a metal alloy coating, characterized in that the wire coating consists of a zinc/cobalt alloy wherein the cobalt content is lower than 1%, adhesion promoters being added to the elastomeric material forming said matrix in order to promote adhesion of same to said reinforcing wires.

Advantageously said adhesion promoters comprise cobalt neodecanate.

Further features and advantages will become more apparent from the following detailed description, given for illustration purposes only, of a preferred embodiment of a surface-treated wire to produce composite elements of elastomeric material and the process for manufacturing said wire, in accordance with the present invention.

In the following description reference will be made to the enclosed table reproducing the results of comparison tests carried out on wires and cords made in accordance with the present invention and on other wires and relevant cords made according to the known art.

The wire in reference is made of steel, preferably of the high tensile type, having a carbon content in the range of 0.6% to 0.9%, and it is provided with a surface coating of a metal alloy having a dual function: that of preventing the wire corrosion and that of promoting adhesion to a matrix of elastomeric material into which the wire will be incorporated, in order to form a composite-material structural element to be used for example in making structural components for tyres and the like.

Since the surface-treated wire is to be submitted to drawing operations, it is also indispensable for the coating to give the wire optimal features in terms of drawing capability.

In accordance with the present invention, in an original manner it is provided that the above surface coating should consist of a zinc/cobalt alloy with a cobalt content not higher than 1% and preferably not higher than 0.5%.

Still in accordance with the invention, said coating is formed by an electrodeposition process in which said alloy is deposited on the wire surface. More particularly, in the process for the manufacture of said surface-coated wire, the wire continuously fed from a reel, is submitted, upon an optional pickling step in sulphuric acid, to an electrolytic bath containing cobalt sulphate and zinc sulphate, in order to achieve the zinc/cobalt alloy deposition on the wire surface.

Preferably, such an electrolytic bath is made up of an aqueous solution containing zinc sulphate heptahydrate to an amount included between 600 and 630 g/l, cobalt sulphate heptahydrate to an amount included between 100 and 110 g/l, as well as sodium sulphate to an amount included between 70 and 80 g/l. Preferably, the pH of the electrolytic bath at a temperature of 55°C has a value included between 1.5 and 2.5. More particularly, the electrolytic bath acidity is preferably adjusted by means of a concentration of H₂SO₄, so as to maintain the predetermined pH value at the predetermined temperature.

The temperature of the electrolytic bath, density of the cathodic current applied to the wire being worked and longitudinal feeding rate of the wire (and consequently the residence time of the wire in the electrolytic bath) have values the adjustments of which depend on each other, for the purpose of accomplishing the zinc/cobalt alloy deposition according to the desired modalities.

In accordance with a preferential solution, the electrolytic bath is maintained to a temperature included between 25°C and 35°C and the metal wire being worked runs through the electrolytic bath at a rate in the range of 15 to 25 m/min, the residence time of the wire in the bath being included between 5 and 15 seconds.

In such a preferential solution, the density of the cathodic current applied to the wire is included between 30 and 40 A/dm².

The main parameters relating to the accomplishment of the electrodeposition process according to a preferential exemplary solution of the invention, given just as an indication, are reproduced hereinafter:

- overall volume of the electrolytic bath: 290 l
- bath composition: ZnSO₄ x 7H₂O = 615 g/l
- CoSO₄ x 7H₂O = 105 g/l
- Na₂SO₄ = 75 g/l
- temperature of the electrolytic bath = 30°C
- density of the cathodic current = 34 A/dm²
- feed rate of the wire = 18 m/min

- residence time of the wire in the electrolytic bath = 10 seconds.

In accordance with an alternative embodiment, the electrolytic bath is maintained to a temperature in the range of 50°C to 60°C, and the wire being worked runs through the electrolytic bath at a rate of 40 to 60 m/min, the residence time of the wire in the electrolytic bath being included between 2 and 6 seconds.

In the alternative embodiment, the density value of the cathodic current applied to the wire is included between 65 and 85 A/dm².

Still by way of example, the fundamental parameters of such a possible alternative version of the process of the invention are also reproduced hereinafter:

- overall volume of the bath: 290 l
- bath composition: $\text{ZnSO}_4 \times 7\text{H}_2\text{O}$ = 620 g/l
 $\text{CoSO}_4 \times 7\text{H}_2\text{O}$ = 125 g/l
 Na_2SO_4 = 75 g/l
- temperature of the electrolytic bath = 55°C
- density of the cathodic current = 75 A/dm²
- feed rate of the wire = 50 m/min
- residence time of the wire in the electrolytic bath = 5 seconds.

In accordance with the present invention, it has been found that the electrodeposition process carried out according to the above description gives rise to a cobalt concentration at the areas closer to the bare wire surface. In the thickness of the coating layer formed as a result of the electrodeposition on the wire not yet drawn, which in a preferential solution has a value in the range of 1 µm to 6 µm, two Co concentration gradients are defined: in the radially innermost area, in contact with the bare wire, having a thickness included between 0.1 nm and 0.4 nm, the cobalt content is in the range of 2% to 3%, whereas in the overlying area, the radially outermost one, the cobalt content is in the order of 0.4% and at all events lower than 0.5%.

Still in accordance with the process in reference, the wire first exhibiting a diameter included between 1.2 mm and 1.6 mm is submitted after formation of the coating layer, to a drawing step following which the coated wire diameter is brought to a value included between 0.10 mm and 0.50 mm. In addition, as a result of drawing, the thickness of the coating layer is brought from the starting value included between 1 µm and 6 µm, to a final value included between 0.1 µm and 0.6 µm.

After the foregoing it will be apparent that the wire made in accordance with the present invention exhibits excellent qualities in terms of drawing capability, by virtue of the low cobalt concentration present in the coating layer, and in particular at the peripheral areas of said layer which are mostly concerned with phenomena of surface friction and wear due to the passage of same through the drawing machines. In this connection it is to be pointed out that, as can be seen in the phase diagram of zinc/cobalt binary alloys (Hansen and Anderko 1958), for cobalt contents lower than 1%, and preferably lower than 0.5%, a good drawing capability of the wire can be achieved because the coating layer alloy only has the α phase which is stable for cobalt contents up to 0.5%. On the contrary, cobalt contents higher than 1% will give rise to the Γ phase exhibiting a high hardness and therefore low-quality features in terms of drawing capability.

Therefore, the wire obtained in accordance with the present invention is free from all problems usually found in wires coated, according to the known art, with a double nickel/cobalt or cobalt/zinc layer and, more generally, in wires coated with zinc/cobalt alloys in which the cobalt content is greater than 1%.

In addition, the wire in reference exhibits surprising qualities of corrosion strength, in spite of the low cobalt content present in the coating layer.

It will be noted in fact that the greater cobalt concentration at the area immediately close to the bare wire surface obtained by the specific electrodeposition process gives rise to a greatly higher corrosion strength than usually expected, taking into account the low cobalt content present on an average in the metal alloy constituting the coating layer as a whole.

In conclusion, a remarkable corrosion strength is achieved, comparable to that of the wires coated with metal alloys having a cobalt content well above 1%, thus eliminating all drawbacks present in wires coated with brass or copper alloys which have a low corrosion strength due to the degradation of the steel/coating layer interface produced by the galvanic currents.

In addition, the wire in reference surprisingly promotes the rubber/metal attachment quality to the ends of making composite materials by insertion of wires or reinforcing metal cords made in accordance with the invention in an elastomeric matrix.

It will be recognized that, in accordance with another feature of the invention, the rubber/metal attachment quality can be considerably improved if appropriate trivalent or pentavalent adhesion promoters are added to the elastomeric

matrix, such as the cobalt neodecanate.

Thus all problems typically found when wires coated with brass or copper alloys are used, are eliminated, which alloys give rise to a great decay of the rubber/metal attachment value due to the copper ion migration in the elastomeric matrix.

5 The table below emphasizes the drawing capability, rubber/metal adhesion and corrosion strength features exhibited by the wires and cords of the invention as compared with those of other wires and cords made in accordance with the known art, taking the features of a conventional brass-coated wire as the touchstone.

For a better comprehension, it is pointed out that in said table the features found with reference to the brass-coated wires and cords have been allocated a value of 100.

10 First of all, with reference to the drawing capability features, the annexed table highlights that well-known wires coated with a zinc/cobalt alloy in which the cobalt content is in the order of 4% and those coated with a double Zn/Co or Zn/Ni layer respectively have a coating loss percentage (column A) four times and twice that of the brass-coated wires, by "loss percentage" meaning the percent amount of material by weight which is taken away from the coating layer as a result of drawing. In the wire made according to the present invention, the loss percentage substantially
15 corresponds to that of the brass-coated wires.

Still with reference to the drawing capability, it will be noted that the number of wire breakages by amount of drawn wire (column B) occurring on the zinc-cobalt coated wires having a cobalt content of 4% and the zinc/cobalt or zinc/nickel double layered wires was respectively in the order of three times and twice that occurred in brass-coated wires, the drawing conditions being equal.

20 On the contrary, the wire made in accordance with the present invention exhibits the same amount of breakages as the brass-coated wire.

As regards the adhesion quality, it is pointed out that it has been tested by evaluating the force necessary for extracting a cord length of the 1x4x0.25 type (four wires with a diameter of 0.25 mm twisted together) from a sample blend in which said cord is incorporated (a test done according to ASTM D-2229 standard).

25 Such a test has been carried out both on samples directly coming from the vulcanization step of the composite material (column C) and on samples previously submitted to an aging process (Column D), consisting in keeping the samples 8 days in a climatic chamber having a humidity content of 90%, and a temperature of 65°C, according to the above mentioned ASTM standard.

30 The test enables the qualitative degradation to adhesion resulting from natural aging of the tyres in use to be evaluated.

Due to the very bad drawing capability of the wires having a cobalt content equal to 4%, it has been impossible to make wires thin enough to enable their use for producing cords designed to carry out comparative tests relating to adhesion resistance and corrosion strength within the composite element.

35 As can be seen, the cord formed of wires coated with a double zinc/cobalt or zinc/nickel layer shows, immediately after vulcanization, a lower attachment level than a cord formed of brass-coated wires. However the attachment level offered by this type of known wires keeps almost constant over time, so that, after aging, it has the same value as that offered by cords formed of brass-coated wires, as said cords undergo a qualitative decay as a result of said aging. The wires manufactured according to the present invention exhibit attachment levels similar to those of the cords having brass-coated wires, both after the vulcanization step and after said aging.

40 As regards the corrosion strength (Column E), as measured by evaluating the rust amount present on a treated wire in a salty environment according to ASTM-B117/73 standard, it is possible to find that both wires made according to the invention and wires coated with a zinc/cobalt or zinc/nickel double layer show a strength 50 times higher than that of the brass-coated wires.

45 The corrosion strength has been also evaluated on a series of four motor-vehicle tyres, size 180/60R14, by machine tests and not by road tests, measuring the corrosion spreading in time.

More particularly, each tyre provided with a belt comprising a pair of strips of rubberized fabric reinforced with said cords type 1x4x0.25, has been rotated on a roller test bench at a speed of 80 km/h for a period of time of 100 hours (Column F) and 200 hours (Column G).

50 At the equatorial plane of the tyre six holes with a diameter of 1 mm have been produced, said holes extending from the radially inner surface of the tread to the area included between the two belt strips; then a saline solution containing 125 g of salt (NaCl) in half a litre of water has been introduced into the tyre.

At the end of the test the tread has been taken away from the tyre and the qualitative evaluation of the rubberizing state of the belt cords has been carried out.

55 The presence of bare cords, that is devoid of rubber, has been ascribed to the rubber/metal bond decay due to the migration of the saline solution along the cord.

In the table below one can see that the corrosion strength in the cords having wires according to the invention is 30 times higher than that of the cords having brass-coated wires after a 100 hour test, and becomes 50 times higher after a 200 hour test, thanks to a lower propagation velocity of the corrosion.

TABLE

Wire Coating	Wire drawing capability		Rubber/Metal Attachment Level		Corrosion on a wire	strength on a tyre	
	A	B	C	D	E	F	G
Brass	100	100	100	100	100	100	100
Zn/Co \geq 4%	400	300	=	=	=	=	=
Zn/Co-Zn/Ni	200	200	80	100	5000	=	=
Zn/Co < 1%	100	100	100	100	5000	3000	5000

Claims

1. A surface-treated steel wire, suitable to be used for reinforcing composite elements of elastomeric material and provided with a surface coating layer of a metal alloy, characterized in that said coating consists of a zinc/cobalt alloy having a cobalt content lower than 1%.
2. A wire according to claim 1, characterized in that said coating layer is obtained by electrodeposition of said alloy on the surface of said bare wire.
3. A wire according to claim 1, characterized in that the cobalt content in the coating layer is lower than 0.5%.
4. A wire according to claim 1, characterized in that said coating layer has a thickness included between 0.1 μm and 0.6 μm .
5. A wire according to claim 1, characterized in that in said coating layer the cobalt is distributed in an uneven manner in two different concentration levels, a first level included between 2% and 3% at the radially inner area directly in contact with the bare wire and a second level lower than 0.5% in the radially outer area overlying the first area.
6. A wire according to claim 5, characterized in that the thickness of the radially inner area having a cobalt concentration gradient included between 2% and 3%, is in the range of 0.1 nm to 0.4 nm.
7. A wire according to claim 1, characterized in that the steel has a carbon content included between 0.6% and 0.9%.
8. A wire according to claim 4, characterized in that it has a diameter in the range of 0.10 mm to 0.50 mm.
9. A process for making a surface treated wire, especially adapted for use in composite elements of elastomeric material, characterized in that it comprises the step of:
 - immersing the wire into an electrolytic bath containing cobalt sulfate and zinc sulfate, for carrying out a deposition of a zinc/cobalt alloy on the outer surface of the treated wire, said alloy exhibiting a cobalt content lower than 1%.
10. A process according to claim 1, characterized in that the electrolytic bath is made up of an aqueous solution containing zinc sulfate heptahydrate in an amount included between 600 and 630 g/l, cobalt sulfate heptahydrate in an amount included between 100 and 110 g/l, as well as sodium sulfate in an amount included between 70 and 80 g/l.
11. A process according to claim 10, characterized in that the electrolytic bath is maintained to a temperature in the range of 25° to 35°C and is passed through by the wire being worked at a rate of 15 to 25 meters/minute, the residence time of the wire in the electrolytic bath having a duration of 5 to 15 seconds.
12. A process according to claim 10, characterized in that the electrolytic bath is maintained to a temperature in the range of 50° to 60°C and is passed through by the wire being worked at a rate of 40 to 60 meters/minute, the residence time of the wire in the electrolytic bath having a duration of 2 to 6 seconds.

13. A process according to claim 10, characterized in that the electrolytic bath has a pH included between 1.5 and 2.5, at 55°C, the value of said pH being adjusted by addition of sulphuric acid.
14. A process according to claim 11, characterized in that a cathodic current of a density included between 30 and 40 A/dm² is applied to the wire being worked.
15. A process according to claim 12, characterized in that a cathodic current of a density included between 65 and 85 A/dm² is applied to the wire being worked.
16. A process according to claim 9, characterized in that the thickness of the coating layer present on the wire after the immersion step in the electrolytic bath is included between 1 µm and 6 µm.
17. A process according to claim 9, characterized in that it further comprises at least one drawing step carried out on the wire provided with the coating layer made up of a zinc/cobalt alloy.
18. A process according to claim 17, characterized in that the wire diameter before drawing has a value included between 1.2 mm and 1.6 mm and, after drawing, a value included between 0.10 and 0.50 mm.
19. A process according to claim 18, characterized in that, after drawing, the thickness of the coating layer is included between 0.1 µm and 0.6 µm.
20. A composite element of an elastomeric material reinforced with steel wires and/or cords of steel wires, provided with a surface coating of a metal alloy, characterized in that said coating consists of a zinc/cobalt alloy wherein the cobalt content is lower than 1%, and in that said composite element contains adhesion promoters designed to promote adhesion of the elastomeric material to said reinforcing wires.
21. A composite element according to claim 20, characterized in that said adhesion promoters comprise cobalt neodecanate.
22. A composite element according to claim 20, characterized in that in said coating layer the cobalt is distributed in an uneven manner in two different concentration levels, a first level included between 2% and 3% at the radially inner area directly in contact with the bare wire and a second level lower than 0.5% in the radially outer area overlying the first area.
23. A composite element according to claim 20, characterized in that said coating layer has a thickness included between 0.1 µm and 0.6 µm.

Patentansprüche

1. Oberflächenbehandelter Stahldraht, der für die Verwendung als verstärkende Verbundelemente von elastomerem Material geeignet und mit einer Oberflächenüberzugsschicht aus einer Metalllegierung versehen ist, dadurch gekennzeichnet, daß der Überzug aus einer Zink-Kobalt-Legierung mit einem Kobaltgehalt von weniger als 1% besteht.
2. Draht nach Anspruch 1, dadurch gekennzeichnet, daß die Überzugsschicht durch Elektroabscheidung der Legierung auf der Oberfläche des blanken Drahts erhalten wird.
3. Draht nach Anspruch 1, dadurch gekennzeichnet, daß der Kobaltgehalt in der Überzugsschicht weniger als 0,5% beträgt.
4. Draht nach Anspruch 1, dadurch gekennzeichnet, daß die Überzugsschicht eine Dicke zwischen 0,1 µm und 0,6 µm hat.
5. Draht nach Anspruch 1, dadurch gekennzeichnet, daß das Kobalt in der Überzugsschicht in ungleichförmiger Weise in zwei unterschiedlichen Konzentrationspegeln verteilt ist, wobei ein erster Pegel an dem radial inneren Bereich direkt in Kontakt mit dem blanken Draht zwischen 2% und 3% und ein zweiter Pegel in dem radial äußeren Bereich, der über dem ersten Bereich liegt, weniger als 0,5% beträgt.

6. Draht nach Anspruch 5, dadurch gekennzeichnet, daß die Dicke des radial inneren Bereichs mit einem Kobaltkonzentrationsgradienten zwischen 2% und 3% in dem Bereich von 0,1 nm bis 0,4 nm liegt.
- 5 7. Draht nach Anspruch 1, dadurch gekennzeichnet, daß der Stahl einen Kohlenstoffgehalt zwischen 0,6% und 0,9% hat.
8. Draht nach Anspruch 4, dadurch gekennzeichnet, daß er einen Durchmesser im Bereich von 0,10 mm bis 0,50 mm hat.
- 10 9. Verfahren zur Herstellung eines oberflächenbehandelten Drahts, der insbesondere zur Verwendung in Verbundelementen aus elastomerem Material geeignet ist, dadurch gekennzeichnet, daß es den Schritt aufweist
 - Eintauchen des Drahts in ein elektrolytisches Bad, das Kobaltsulfat und Zinksulfat enthält, um eine Abscheidung einer Zink-Kobalt-Legierung an der Außenfläche des behandelten Drahts durchzuführen, wobei die Legierung einen Kobaltgehalt von weniger als 1% hat.
- 15 10. Verfahren nach Anspruch 1, dadurch gekennzeichnet, daß das elektrolytische Bad aus einer wässrigen Lösung besteht, die Zinksulfatheptahydrat in einer Menge zwischen 600 und 630 g/l, Kobaltsulfatheptahydrat in einer Menge zwischen 100 und 110 g/l sowie Natriumsulfat in einer Menge zwischen 70 und 80 g/l enthält.
- 20 11. Verfahren nach Anspruch 10, dadurch gekennzeichnet, daß das elektrolytische Bad auf einer Temperatur im Bereich von 25°C bis 35°C gehalten und vorn in Behandlung befindlichen Draht mit einer Geschwindigkeit von 15 bis 25 m/min durchquert wird, wobei die Verweilzeit des Drahtes in dem elektrolytischen Bad eine Dauer von 5 bis 15 s hat.
- 25 12. Verfahren nach Anspruch 10, dadurch gekennzeichnet, daß das elektrolytische Bad auf einer Temperatur im Bereich von 50°C bis 60°C gehalten wird und von dem in Behandlung befindlichen Draht mit einer Geschwindigkeit von 40 bis 60 m/min durchquert wird, wobei die Verweilzeit des Drahtes in dem elektrolytischen Bad eine Dauer von 2 bis 6 s hat.
- 30 13. Verfahren nach Anspruch 10, dadurch gekennzeichnet, daß das elektrolytische Bad einen pH-Wert zwischen 1,5 und 2,5 bei 55°C hat, wobei der pH-Wert durch Zugabe von Schwefelsäure eingestellt wird.
- 35 14. Verfahren nach Anspruch 11, dadurch gekennzeichnet, daß ein kathodischer Strom mit einer Dichte zwischen 30 und 40 A/dm² an den in Behandlung befindlichen Draht angelegt wird.
15. Verfahren nach Anspruch 12, dadurch gekennzeichnet, daß ein kathodischer Strom mit einer Dichte zwischen 65 und 85 A/dm² an den in Behandlung befindlichen Draht angelegt wird.
- 40 16. Verfahren nach Anspruch 9, dadurch gekennzeichnet, daß die Dicke der auf dem Draht nach dem Eintauchschritt in das elektrolytische Bad vorhandenen Überzugsschicht zwischen 1 µm und 6 µm liegt.
17. Verfahren nach Anspruch 9, dadurch gekennzeichnet, daß es weiterhin wenigstens einen Ziehschritt aufweist, der an dem Draht ausgeführt wird, der mit der aus einer Zink-Kobalt-Legierung hergestellten Überzugsschicht versehen ist.
- 45 18. Verfahren nach Anspruch 17, dadurch gekennzeichnet, daß der Drahtdurchmesser vor dem Ziehen einen Wert zwischen 1,2 mm und 1,6 mm und nach dem Ziehen einen Wert zwischen 0,10 und 0,50 mm hat.
- 50 19. Verfahren nach Anspruch 18, dadurch gekennzeichnet, daß nach dem Ziehen die Dicke der Überzugsschicht zwischen 0,1 µm und 0,6 µm liegt.
- 55 20. Verbundelement eines elastomeren Materials, das mit Stahldrähten und/oder Korden aus Stahldrähten verstärkt ist, die mit einem Oberflächenüberzug aus einer Metalllegierung versehen sind, dadurch gekennzeichnet, daß der Überzug aus einer Zink-Kobalt-Legierung besteht, wobei der Kobaltgehalt weniger als 1% beträgt, und daß das Verbundelement Haftpromotoren enthält, die so ausgelegt sind, daß die Haftung des elastomeren Materials an den Verstärkungsdrähten begünstigt wird.

21. Verbundelement nach Anspruch 20, dadurch gekennzeichnet, daß die Haftpromotoren Kobaltneodecanat aufweisen.
- 5 22. Verbundelement nach Anspruch 20, dadurch gekennzeichnet, daß in der Überzugsschicht das Kobalt in ungleichförmiger Weise in zwei unterschiedlichen Konzentrationspegeln verteilt ist, wobei ein erster Pegel an dem radial inneren Bereich direkt in Kontakt mit dem blanken Draht zwischen 2% und 3% und ein zweiter Pegel in dem radial äußeren Bereich, der über dem ersten Bereich liegt, weniger als 0,5% beträgt.
- 10 23. Verbundelement nach Anspruch 20, dadurch gekennzeichnet, daß die Überzugsschicht eine Dicke zwischen 0,1 µm und 0,6 µm hat.

Revendications

- 15 1. Fil métallique en acier traité en surface, pouvant être utilisé pour renforcer des éléments composite en matériau élastomère et comportant une couche superficielle de revêtement en alliage métallique, caractérisé en ce que ledit revêtement est un alliage de zinc/cobalt qui contient moins de 1% de cobalt.
- 20 2. Fil métallique selon la revendication 1, caractérisé en ce que ladite couche de revêtement est obtenue par dépôt électrolytique dudit alliage sur la surface dudit fil métallique nu.
3. Fil métallique selon la revendication 1, caractérisé en ce que la quantité de cobalt dans la couche de revêtement est inférieure à 0,5%.
- 25 4. Fil métallique selon la revendication 1, caractérisé en ce que ladite couche de revêtement a une épaisseur comprise entre 0,1 µm et 0,6 µm.
5. Fil métallique selon la revendication 1, caractérisé en ce que le cobalt est réparti dans ladite couche de revêtement de manière irrégulière avec deux niveaux de concentration différents, un premier niveau compris entre 2% et 3% en la région radialement intérieure qui est directement en contact avec le fil métallique nu et un deuxième niveau inférieur à 0,5% dans la région radialement extérieure qui recouvre la première région.
- 30 6. Fil métallique selon la revendication 5, caractérisé en ce que l'épaisseur de la région radialement intérieure ayant un gradient de concentration de cobalt compris entre 2% et 3% se situe dans la fourchette de 0,1 nm à 0,4 nm.
- 35 7. Fil métallique selon la revendication 1, caractérisé en ce que l'acier a une teneur en carbone comprise entre 0,6% et 0,9%.
- 40 8. Fil métallique selon la revendication 4, caractérisé en ce qu'il a un diamètre dans la fourchette de 0,10 mm à 0,50 mm.
9. Procédé de fabrication d'un fil métallique traité en surface, particulièrement adapté à une utilisation dans des éléments composites en matériau élastomère, caractérisé en ce qu'il comprend l'étape consistant à immerger le fil métallique dans un bain électrolytique contenant du sulfate de cobalt et du sulfate de zinc, pour effectuer un dépôt d'alliage zinc/cobalt sur la surface extérieure du fil métallique traité, ledit alliage ayant une teneur en cobalt inférieure à 1%.
- 45 10. Procédé selon la revendication 9, caractérisé en ce que le bain électrolytique est fait d'une solution aqueuse contenant du sulfate de zinc heptahydraté en une quantité comprise entre 600 et 630 g/l, du sulfate de cobalt heptahydraté en une quantité comprise entre 100 et 110 g/l, ainsi que du sulfate de sodium en une quantité comprise entre 70 et 80 g/l.
- 50 11. Procédé selon la revendication 10, caractérisé en ce que le bain électrolytique est maintenu à une température dans la fourchette de 25 à 35°C et est traversé par le fil métallique à une vitesse de 15 à 25 m/mn, le temps de résidence du fil métallique dans le bain électrolytique étant compris entre 5 et 15 secondes.
- 55 12. Procédé selon la revendication 10, caractérisé en ce que le bain électrolytique est maintenu à une température dans la fourchette de 50 à 60°C et est traversé par le fil métallique à une vitesse de 40 à 60 m/mn, le temps de

résidence du fil métallique dans le bain électrolytique étant compris entre 2 et 6 secondes.

13. Procédé selon la revendication 10, caractérisé en ce que le bain électrolytique a un pH compris entre 1,5 et 2,5 à 55°C, la valeur dudit pH étant ajustée par addition d'acide sulfurique.

14. Procédé selon la revendication 11, caractérisé en ce qu'un courant cathodique d'une densité comprise entre 30 et 40 A/dm² est appliqué au fil métallique en cours de traitement.

15. Procédé selon la revendication 12, caractérisé en ce qu'un courant cathodique d'une densité comprise entre 65 et 85 A/dm² est appliqué au fil métallique en cours de traitement.

16. Procédé selon la revendication 9, caractérisé en ce que l'épaisseur de la couche de revêtement présente sur le fil métallique après l'étape d'immersion dans le bain électrolytique est comprise entre 1 µm et 6 µm,

17. Procédé selon la revendication 9, caractérisé en ce qu'il comprend en outre au moins une étape d'étirage effectuée sur le fil comportant la couche de revêtement en alliage de zinc/cobalt.

18. Procédé selon la revendication 17, caractérisé en ce que le diamètre du fil métallique avant étirage a une valeur comprise entre 1,2 mm et 1,6 mm et, après étirage, une valeur comprise entre 0,10 et 0,50 mm.

19. Procédé selon la revendication 18, caractérisé en ce que, après étirage, l'épaisseur de la couche de revêtement est comprise entre 0,1 µm et 0,6 µm.

20. Élément composite en matériau élastomère renforcé par des fils d'acier et/ou des câbles de fils d'acier comportant un revêtement superficiel d'alliage métallique, caractérisé en ce que ledit revêtement est un alliage de zinc/cobalt dans lequel la quantité de cobalt est inférieure à 1%, et en ce que ledit élément composite contient des agents favorisant l'adhérence, conçus pour faciliter l'adhérence du matériau élastomère auxdits fils métalliques de renfort.

21. Élément composite selon la revendication 20, caractérisé en ce que lesdits agents favorisant l'adhérence comprennent du néodécane de cobalt.

22. Élément composite selon la revendication 20, caractérisé en ce que le cobalt est réparti dans ladite couche de revêtement de manière irrégulière avec deux niveaux de concentration différents, un premier niveau compris entre 2% et 3% en la région radialement intérieure qui est directement en contact avec le fil métallique nu et un deuxième niveau inférieur à 0,5% dans la région radialement extérieure qui recouvre la première région.

23. Élément composite selon la revendication 20, caractérisé en ce que ladite couche de revêtement a une épaisseur comprise entre 0,1 µm et 0,6 µm.